



Coiled Tubing String Failures – Past and Present

ICoTA Canada Breakfast Technical Session

May 30th 2018

Tomas Padron – Coiled Tubing Research & Engineering



Outline

- What is a CT string failure and examples
- Why doing CT string failure analyses
- CT string failure analysis process
- CT failure statistics
- Main ideas

CT String Failures

- Knowledge and control of fatigue performance
- Improvements in materials and manufacturing processes



Within the company:

- CT failures are analyzed and causes established
- CT failures statistical data

What is a CT Failure?

- CT failure:
 - Loss of pressure integrity of the tubing during service and before the predicted fatigue life has been exceeded.
 - Any condition that renders the string not safe to be used.

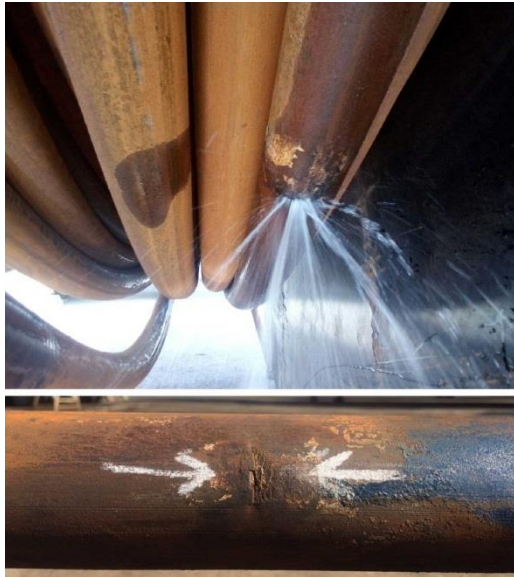


It's only a
failure
if you don't
learn
something

What is a CT Failure? – Examples

Pinhole

POOH – PLT run



2-3/8" OD – CT90

Partial Fracture

RIH – Milling



2-3/8" OD – CT100

Total Fracture

Pulling to free string
Cleanout



2" OD – CT90

What is a CT Failure? – Other examples

Burst

Pressure testing



1-3/4" OD – CT90

Extensive Damage

POOH Logging job



1-3/4" OD – CT90

Collapse

RIH Cleanout



2-3/8" OD – CT100

???

New string - Inspection



2-3/8" OD – CT80

Why doing CT strings failure analyses?

- Make decisions / take corrective actions based on data and not guesses or “gut feelings”



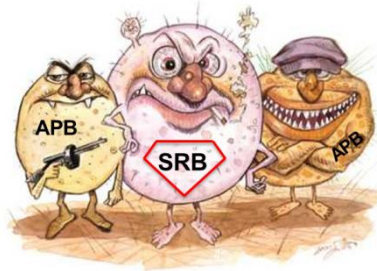
Why doing CT strings failure analyses? – Example

Failure Sequence-Date	Manufacturer	Diameter (in.)	Grade	Days of Service	Runs – Wells	Max. SFL used (%)
First April 9 th 2013	A	2	90	26	22 - 7	36
Second May 6 th 2013				47	25 - 6	36
Third May 18 th 2013	B			24	14 - 6	29
Fourth May 20 th 2013				14	11 - 4	17
Fifth July 5 th 2013	A			41	22 - 7	50
Sixth July 24 th 2013				11	9 - 3	34

“Solutions” initially proposed without any failure analysis:

- “Bad quality” pipe – change manufacturer
- Change the string Grade to YYY
- Limit the fatigue life used to XX%
- Others

All six failures were associated to MIC (fluid contaminated with bacteria)



Real solutions:

- Treatment of surface equipment
- Treatment of circulating fluids
- Between-wells stagnant fluids treatment

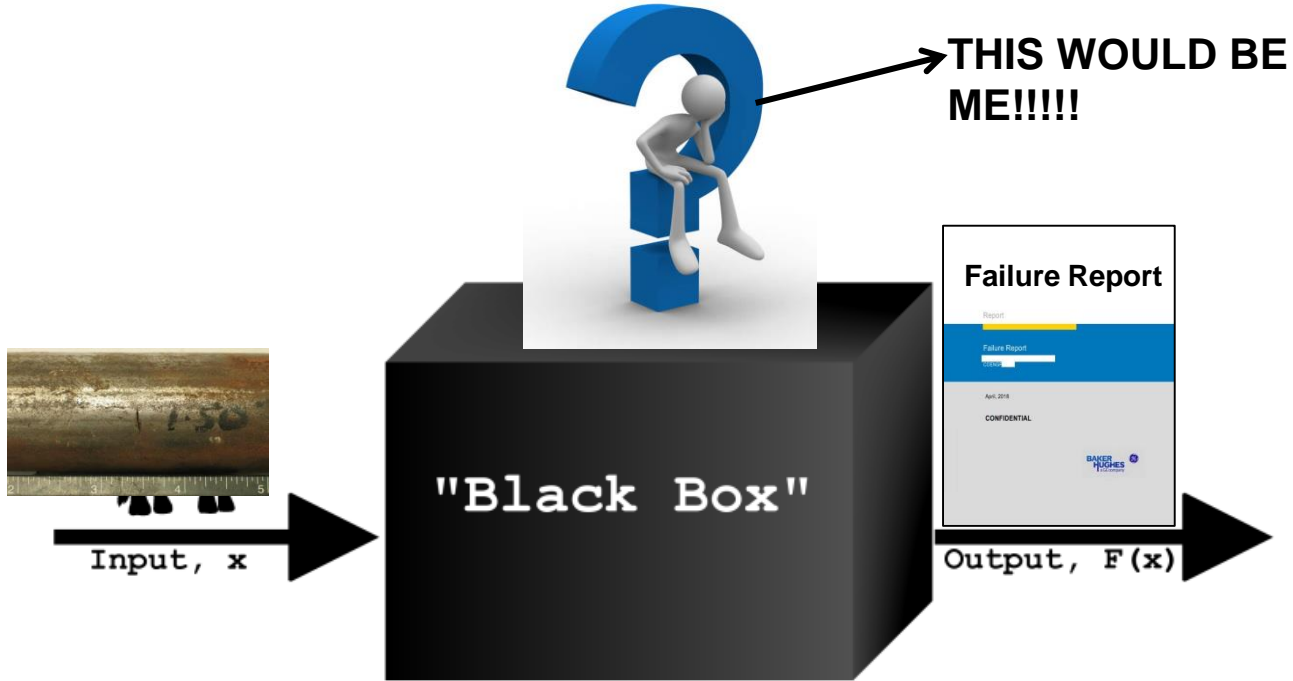
CT string failure analysis process

CT failure analysis:

Logical process of examination to establish the failure cause(s) based on evidence collected and the use of engineering principles.



CT string failure analysis process



Failure analyses are not done with a black box

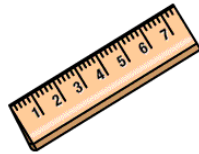
CT string failure analysis process

We don't use crystal balls either !!!!



CT string failure analysis process

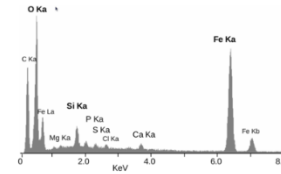
- Most common CT failure analyses include the following stages:
 - Sample(s) collection/preservation
 - Collection of data regarding failure/CT string
 - Visual/stereoscopic examination
 - Dimensional inspection
 - Metallographic analysis
 - Results analysis and report preparation



CT string failure analysis process

- Some additional analyses that are required for some particular cases:

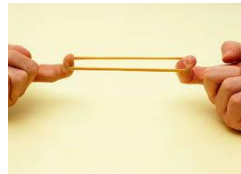
- Energy-Dispersive Spectroscopy (EDS)



- Scanning Electron Microscope (SEM) Fractography



- Tension tests



- Others: Charpy test, corrosion tests, etc.



CT string failure analysis process – Sample(s) collection / preservation

1.2 Sample Collection

1. Cut at least 1 foot on either side of the failure location. Use a tubing cutter or saw to do this, NOT a cutting torch. The up-hole end should be labeled U1 and the downhole end D1.
2. Cut 7 to 8 foot samples on either side. Use a tubing cutter or saw to do this, NOT a cutting torch. Each end of the sample should be labeled U2 - U3 and D2 - D3.

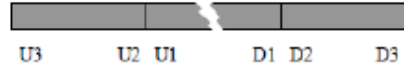



Figure - 1 Required Sample Marking



Level: L2 - Procedure Tier: GLB - Global
 Document Type: Procedure
 Sub Element: Operations
 Doc Number: OPS-GLB-En-101452
 Rev: A
 Effective Date: 3/4/2015

2.5.3.8 Procedure for Collection of Field Samples of Coiled Tubing In The Event of a Failure

Revision History					
Rev.	RDR	Amendment Details	Reviewer	Approver	Effective Date
A	-	Initial Release - J Wint	Lant, Keith	Moreira Neto, Lino	3/4/2015
Three Previous Revisions					

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CT string failure analysis process – Data collection (Failure/String)

Data about the failure: date, failure type, job, operation, well and customer, tubing depth, any additional information



Failure Report

Date Printed: 5/11/2018

Reel Number: TA-22022	String Length: 21,047.00 ft
String Number:	Outside Diameter: 1.75 in
String Description: Tapered	Current Volume: 40.567 bbl
String Material:	District/Boat:
Accumulated Fatigue: 1.320 %	Total RIH Distance: 41,293.00 ft

Cause Of Failure:		9/25/2017 10:00:54 AM	
Failure Type	Pin Hole	Operation	Stationary
Failure Place	On the Reel	Job Type	Unspecified
Tubing Depth	13,385.83 ft	Job Ticket No.	
RIH Weight	0.00 lb	Location	
POOH Weight	0.00 lb	Customer	
Overall Layoff Weight	0.00 lb	Reel No.	TA-22022
CT Pressure	0.00 psi g	Core Diameter	90.000 in
WH Pressure	0.00 psi g	Core Width	86.00 in
Fluid Rate	0.00 bbl/min	Flange Diameter	156.000 in
Fluid Type	Water Based		

Comments: Leak was found when fluid was pumped into CT string for pressure testing. Failure of string to be defined after the metallurgic test.

CT string failure analysis process – Data collection (Failure/String)

Manufacturer's Mill Certificate

QTR Form No. 17
3/20/2015 (04/1)

WELD LOCATION RECORD AND MATERIAL CERTIFICATE

NOV Quality Tubing

Weld Location Diagram:

Spool#	Mat. length	Mat. Yield	Yield Strength	Yield	Tensile	Tensile	Tensile	Tensile	Yield	Rockwell	Chemical Analysis												
Weight	ft	lb	MPa	ksi	MPa	ksi	ksi	ksi	ksi	HRC	C	Mn	P	S	Si	Cr	Ni	Mo	Fe				
13	130000437	156	156	625	633	59988	223038	105000	114000	1.18	28.3	24	HRC	0.22	1.470	0.015	0.010	0.30	0.580	0.230	0.070	0.063	0.046
12	130000433	156	156	1470	2088	59988	223038	105000	114000	1.18	28.3	24	HRC	0.22	1.470	0.015	0.010	0.30	0.580	0.230	0.070	0.063	0.046
11	130000429	156	156	1470	2088	59988	223038	105000	114000	1.18	28.3	24	HRC	0.22	1.470	0.015	0.010	0.30	0.580	0.230	0.070	0.063	0.046
10	130000425	156	156	1470	2088	59988	223038	105000	114000	1.18	28.3	24	HRC	0.22	1.470	0.015	0.010	0.30	0.580	0.230	0.070	0.063	0.046
9	130000421	156	156	1443	6489	59988	223038	105000	114000	1.18	28.3	24	HRC	0.22	1.470	0.015	0.010	0.30	0.580	0.230	0.070	0.063	0.046
8	130000418	156	156	1953	8453	59988	183048	105000	113000	1.07	28.2	23	HRC	0.22	1.470	0.015	0.010	0.30	0.580	0.230	0.067	0.062	0.044
7	130000415	156	156	1438	9818	59988	123037	111000	123000	1.18	30.3	28	HRC	0.22	1.460	0.015	0.010	0.30	0.580	0.230	0.080	0.063	0.050
6	130000412	156	156	1909	11948	59988	123037	111000	123000	1.18	30.3	28	HRC	0.22	1.460	0.015	0.010	0.30	0.580	0.230	0.080	0.063	0.050
5	130000409	156	156	1463	12881	59988	123037	111000	123000	1.18	30.3	28	HRC	0.22	1.460	0.015	0.010	0.30	0.580	0.230	0.080	0.063	0.050
4	130000405	156	156	1404	14377	59988	123037	111000	123000	1.18	30.3	28	HRC	0.22	1.460	0.015	0.010	0.30	0.580	0.230	0.080	0.063	0.050
3	130000402	156	156	1483	13840	59988	123037	111000	123000	1.18	30.3	28	HRC	0.22	1.460	0.015	0.010	0.30	0.580	0.230	0.080	0.063	0.050
2	130000399	156	156	1483	13840	59988	123037	111000	123000	1.18	30.3	28	HRC	0.22	1.460	0.015	0.010	0.30	0.580	0.230	0.080	0.063	0.050
1	130000396	156	156	1483	13840	59988	123037	111000	123000	1.18	30.3	28	HRC	0.22	1.460	0.015	0.010	0.30	0.580	0.230	0.080	0.063	0.050
0	130000393	156	156	1327	29312	59988	123037	111000	123000	1.18	30.3	28	HRC	0.22	1.460	0.015	0.010	0.30	0.580	0.230	0.080	0.063	0.050

String Manufactured: 1/14/2013

Orientation: Y BEO

Notes: We hereby certify that the material described herein has been manufactured, tested and inspected satisfactorily in accordance with the requirements of the above specification or applicable acceptance.

Page 1 of 1

Tenaris

Type of Document Form: **WELD LOCATION RECORD**

Customer: **BAKER HUGHES THAILAND**

Product: **BlueCoil™ Technology**

Grade: **HT-125-C**

String Number: **36806-1**

Weight: 1.988, 5.315, 5.980, 6.158, 6.089, 6.217, 5.989, 5.482, 5.482, 5.413, 5.483, 5.511, 6.161

Length: 45.34, 413.00, 84.72, 386.29, 386.24, 405.38, 386.24, 423.67, 426.72, 425.02, 422.18, 428.24, 473.00

Wall Thickness: 280, 254, 254, 254, 254, 254, 254, 254, 254, 254, 254, 254, 254

Spool Size: 160-80

Spool ID No: 8315

SA308S32C030-5A, SA308S32C030-5A, SA308S32C030-5A, SA308S32C030-5A, SA308S32C030-5A, SA308S32C030-5A, SA308S32C030-5A, SA308S32C030-5A, SA308S32C030-5A, SA308S32C030-5A, SA308S32C030-5A, SA308S32C030-5A, SA308S32C030-5A, SA308S32C030-5A

String Number: SA308S32C030-5A

Grade: HT-125-C

Size: 2.05

SALES ORDER NO: 36010037

DATE COMPLETED: 11/18/2015

SHIPPED TO: Baker Hughes, Sidra

P.O. NUMBER: 60272651

TOTAL FOOTAGE: 18,750

TOTAL METERS: 6,687.6

EST: THAIHQ WF: 73,358

DATE COMPLETED 11/18/2015

Tenaris

Type of Document Form: **REPORT OF TEST, INSPECTIONS AND ANALYSIS**

Customer: **BAKER HUGHES SIDRA S.A.L.C.**

Product: **BlueCoil™ Technology**

Grade: **HT-125-C**

String Number: **36806-1**

Customer P.O.: **1CT 0017**

Date Completed: **12/3/15**

String Number: **36806-1**

Customer No: **60272551**

Serial No: **36010037**

Reference: **BlueCoil™ Technology**

Supplemental Testing: Export crate and Anti-roll Blocks

Certification Notes: Filling Type Approved By Date

Repair Notes: Filling Location Raymond Goodman 09/20/13

Signature: *R.D. Goodman*

Manufacturing Dept: Date Spec: 02-19-19

Mill Date 09/18/13

AS MILLED-READY TO SHIP

Order Date: **09/18/13**

Status: **Complete**

Customer: **BAKER HUGHES THAILAND**

Location: **Laemchabang, Thailand**

Req. Date: **07-90**

Grade: **ASTM A666**

Sizing: **3371**

WLR No: **4 of 5**

Dayton: **01-90**

ASTM: **A666**

Diameter: **12.475**

Actual: **12.475**

Hydral: **30**

Duration: **30**

Weld ID: **9819**

WID ID: **9819**

Work Order No: **5634**

Rev: **1**

SO ID: **4387**

Rev: **1**

QC-15-10 Revision: 1 20 Feb-13

GT Product Specification: **Kim Carton Product Testing in accordance with ASTM A370**

(Nondestructive Testing in accordance with ASTM E339)

Strip No.	Mat. length	Mat. Yield	Yield Strength	Yield	Tensile	Tensile	Tensile	Tensile	Yield	Rockwell	Chemical Analysis												
Weight	ft	lb	MPa	ksi	MPa	ksi	ksi	ksi	ksi	HRC	C	Mn	P	S	Si	Cr	Ni	Mo	Fe				
206-0111-128	156	1340	1364	59988	23174	110500	110500	110500	110500	93.1	92.1	92.627	98.833	26.70	27.774	0.015	0.010	0.300	0.580	0.230	0.070	0.063	0.046
206-0111-127	156	2350	4220	59988	23174	110500	110500	110500	110500	93.1	92.1	92.627	98.833	26.70	27.774	0.015	0.010	0.300	0.580	0.230	0.070	0.063	0.046
206-0111-124	156	2360	6620	59988	23174	110500	110500	110500	110500	93.1	92.1	92.627	98.833	26.70	27.774	0.015	0.010	0.300	0.580	0.230	0.070	0.063	0.046
206-0111-122	156	2350	9220	59988	23174	110500	110500	110500	110500	93.1	92.1	92.627	98.833	26.70	27.774	0.015	0.010	0.300	0.580	0.230	0.070	0.063	0.046
K05-1011-1-9A	116	1150	10,110	PAW	5317-1-PG	95.4	93.7	94.415	100,462	26,50	33,664	0.1	0.01	0.009	0.003	0.36	0.28	0.17	0.81	0.16	0.06	0.136	0.038
028-3402-1-1EA	125	1150	11,300	PAW	5317-2-PG	94.3	91.7	95.348	102,150	26,79	33,664	0.1	0.01	0.010	0.003	0.36	0.28	0.16	0.81	0.16	0.06	0.136	0.038
1715-5071-1-5EA	134	1,050	12,400	PAW	5317-3-PG	95.2	92.8	96.280	103,375	26,98	34,486	0.1	0.01	0.010	0.003	0.36	0.27	0.16	0.81	0.16	0.06	0.136	0.038
710-0061-1-4A	145	1,070	13,470	PAW	5317-4-PG	94.4	93.8	94.208	102,000	28,38	36,372	0.1	0.01	0.010	0.003	0.37	0.16	0.17	0.81	0.16	0.06	0.136	0.038
501-0201-1-1EA	156	1,010	14,480	PAW	5317-00-00	96.3	95.9	93.783	100,340	28,89	36,569	0.1	0.01	0.010	0.003	0.36	0.16	0.17	0.81	0.16	0.06	0.136	0.038
K05-1011-1-1E	175	1,210	15,700	-	-	96.6	92.8	97.074	105,124	29,03	33,664	0.1	0.01	0.009	0.003	0.36	0.28	0.17	0.81	0.16	0.06	0.136	0.038

Actual Length: **18,750**

Hint: Milling date gives a good idea on how old was the string

String Manufactured: 1/14/2013

CT string failure analysis process – Data collection (Failure/String)

String records:

- First job date / Most common job
- Average fatigue used / Fatigue used at failure location
- Long term storage periods and corrosion protection activities

Overview Report
Date Printed: 1/15/2018

Well Number: 25726 06 409
String Length: 15,209.00 ft
Current Diameter: 1.25 in
String Description: Regular
Current Volume: 34,501 bbl
String Material: 4010
Accumulated Fatigue: 2.212 %
Total RH Distance: 109,382.00 ft

Well Type Legend

- ✓ Production Well
- Production Well
- Field - Manual Run
- Field - Chased Run
- Slipstream

Tabular String Report

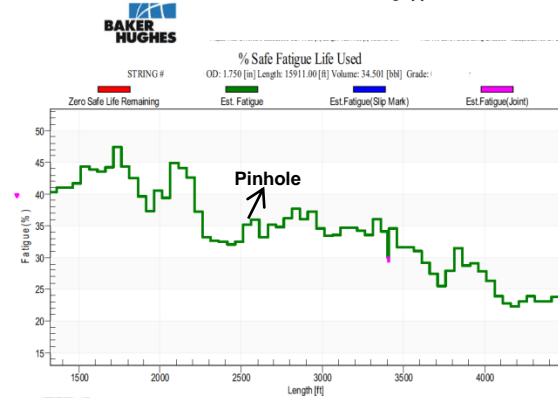
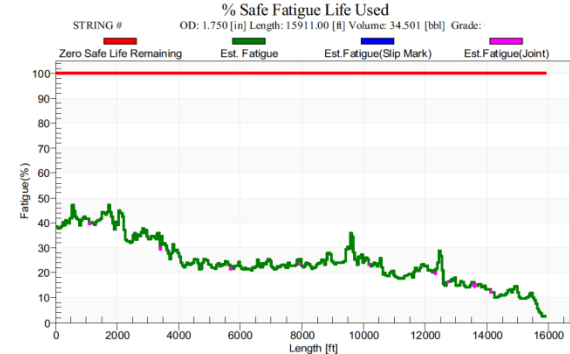
Run #	Run Date	Run Type	Run Length (ft)	Run Volume (bbl)	Run Type	Run Date
1	11/04/00-A	R	15,209.00	34,501.00	Production	2000-11-04
2	11/10/00-B	R	15,209.00	34,501.00	Production	2000-11-10
3	11/16/00-C	R	15,209.00	34,501.00	Production	2000-11-16
4	11/22/00-D	R	15,209.00	34,501.00	Production	2000-11-22
5	11/28/00-E	R	15,209.00	34,501.00	Production	2000-11-28
6	12/04/00-F	R	15,209.00	34,501.00	Production	2000-12-04
7	12/10/00-G	R	15,209.00	34,501.00	Production	2000-12-10
8	12/16/00-H	R	15,209.00	34,501.00	Production	2000-12-16
9	12/22/00-I	R	15,209.00	34,501.00	Production	2000-12-22
10	12/28/00-J	R	15,209.00	34,501.00	Production	2000-12-28

Run History Report

Run #	Well Number	String Type	Run Length (ft)	Run Volume (bbl)	Run Type	Run Date
1	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-11-04
2	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-11-10
3	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-11-16
4	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-11-22
5	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-11-28
6	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-12-04
7	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-12-10
8	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-12-16
9	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-12-22
10	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-12-28

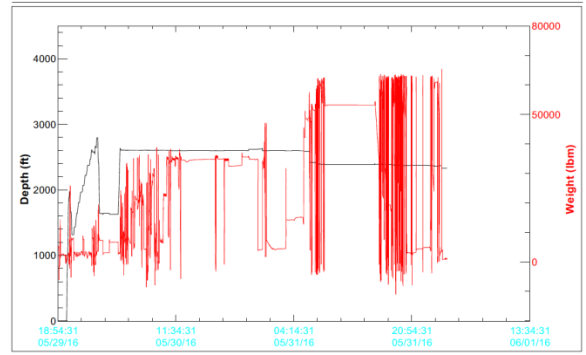
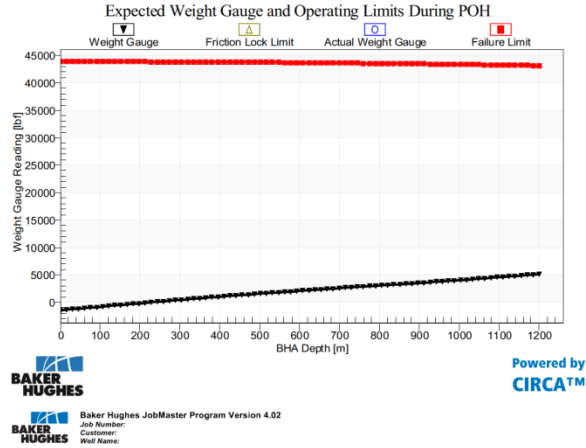
Maintenance History Report

Run #	Well Number	String Type	Run Length (ft)	Run Volume (bbl)	Run Type	Run Date
1	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-11-04
2	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-11-10
3	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-11-16
4	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-11-22
5	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-11-28
6	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-12-04
7	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-12-10
8	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-12-16
9	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-12-22
10	25726 06 409	Regular	15,209.00	34,501.00	Production	2000-12-28

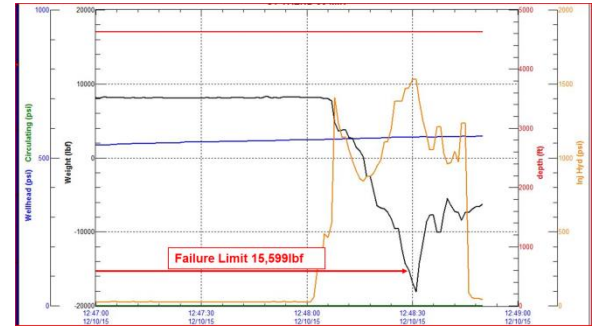


CT string failure analysis process – Data collection (Failure/String)

Job parameters and operational limits (mainly for overload/buckling failures)



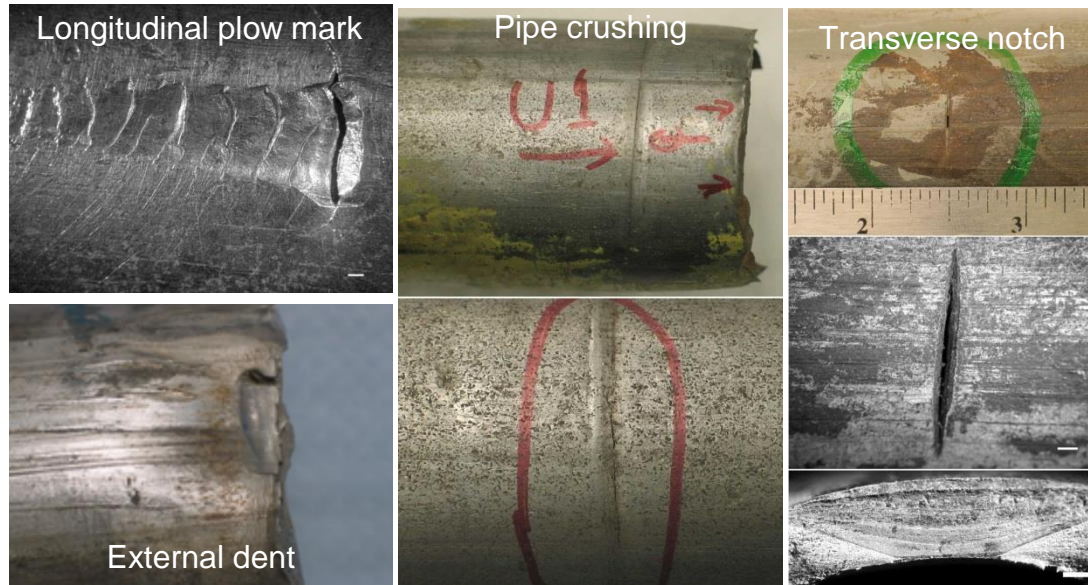
Baker Hughes Job Start: Sunday, May 29, 2016



CT string failure analysis process – Visual/Stereoscopic Examination

- One of the most important stages – In many cases gives good evidence on the cause of the failure – What to look for during this stage?:

Mechanical damage



Visual/Stereoscopic Examination – What to look for?

External Corrosion

Acid job – 2" – CT80

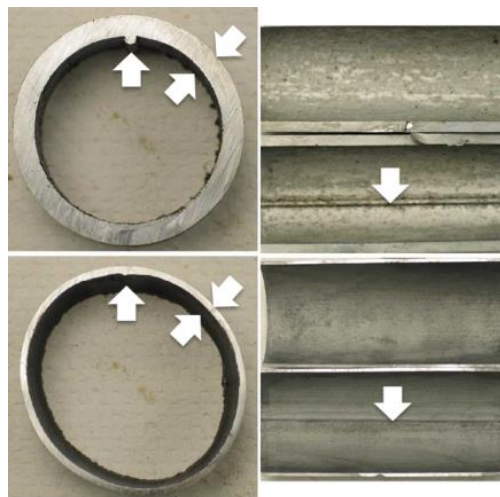


Pressure testing

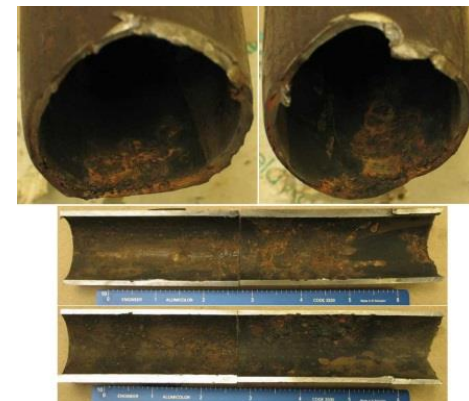


1-3/4" – CT1300

Internal Corrosion



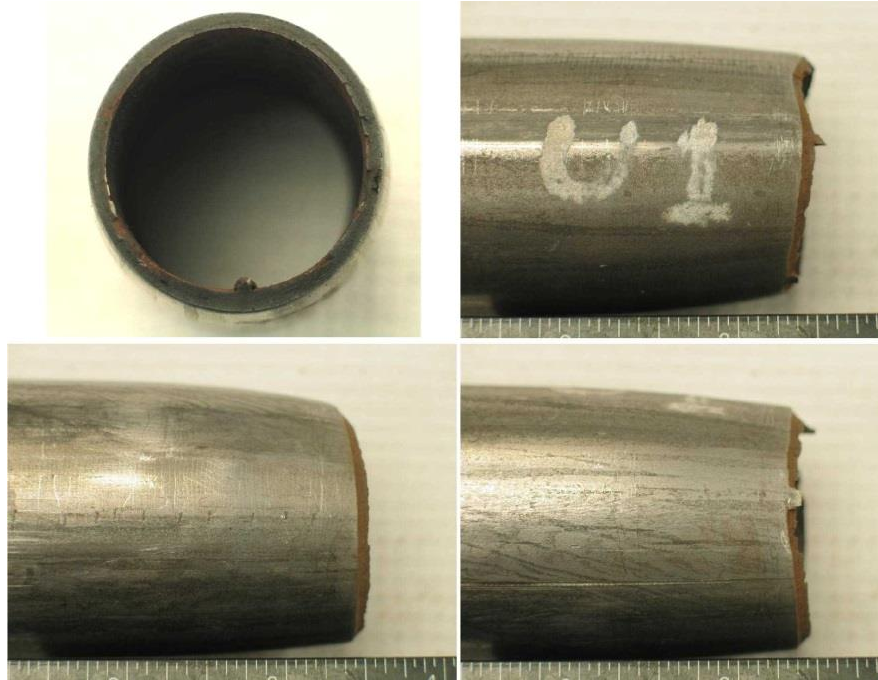
Acid job – 1-1/2" – CT80



N2 jetting – 1-1/2" – CT80

Visual/Stereoscopic Examination – What to look for?

Necking and 45° fracture propagation



Fishing – 2" – CT90

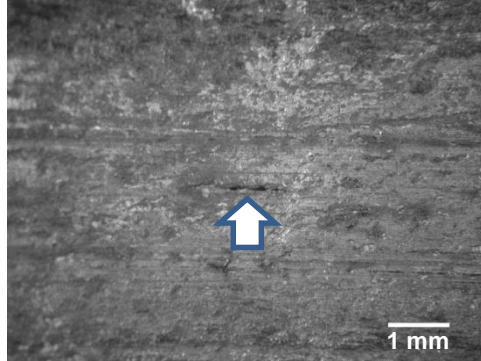
Visual/Stereoscopic Examination – What to look for?

Small longitudinal splits

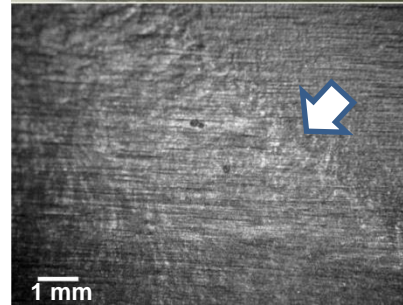
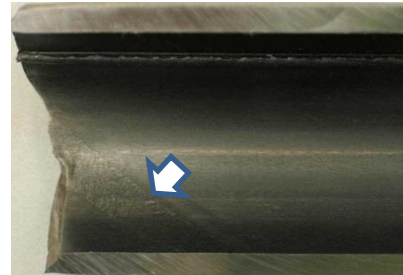
Pressure Testing
2-3/8" – CT100



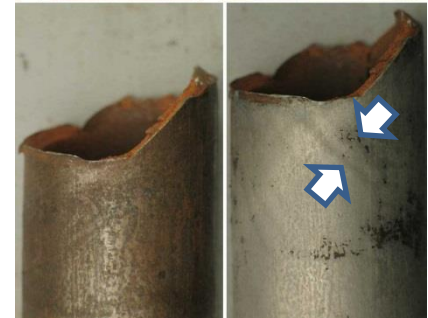
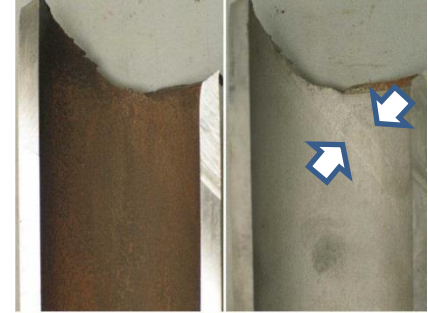
Optiport
2" – CT90



Confirm the presence of a bias weld



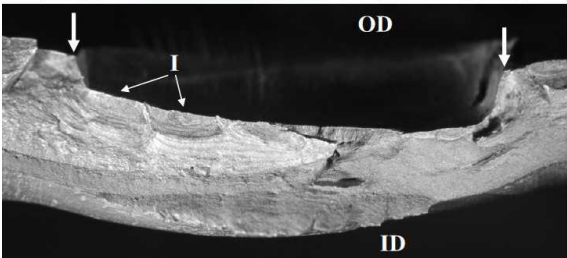
Milling – 2" – CT90



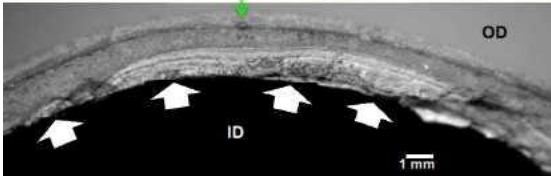
Milling – 2" – CT90

Visual/Stereoscopic Examination – What to look for?

Fracture origin



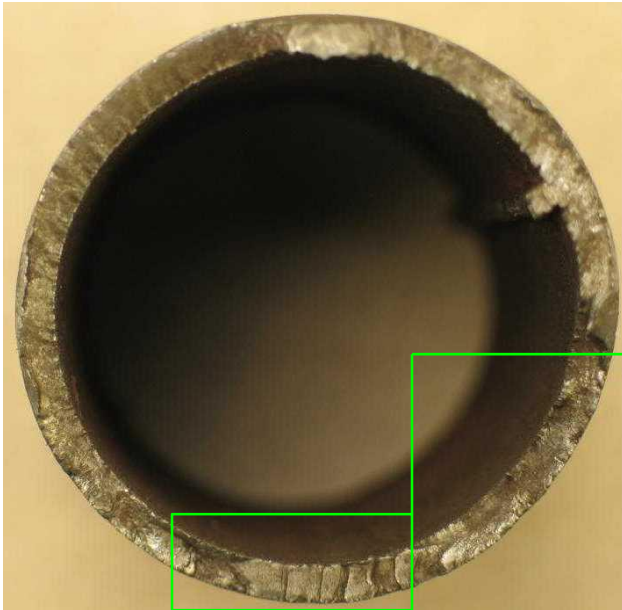
Frac – 2-7/8” – CT70



Milling – 1-1/2” – CT90

Visual/Stereoscopic Examination – What to look for?

Fracture origin



Fishing – 1-3/4" – CT90

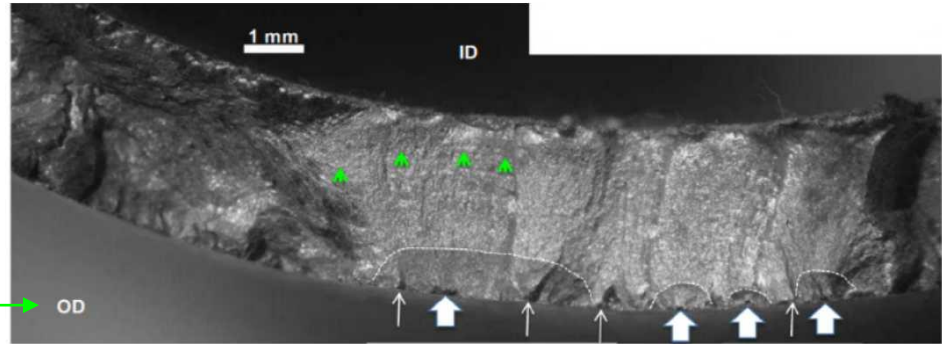


Figure 4. Detailed view of the “flat” portion of the fracture shown in Figure 3b. The following features can be observed:

- Ratchet marks at the outside diameter (small white arrows), indicative of multiple fatigue cracks starting at the outside diameter.
- Thumb nail cracks starting from external pits (darker areas enclosed by dotted lines and block arrows).
- Some light marks concentric towards the OD can be observed (small green arrows), indicating propagation by fatigue from the OD.

All these features indicate that the fracture started at this location (fracture origin) from multiple fatigue cracks that propagated from the outside diameter at external pits.

CT string failure analysis process – Dimensional inspection

Verify the pipe condition regarding OD, ovality, wall thickness.

Acid corrosion



External abrasion



Location	Down-hole end (1)	1	2	3	4	5	6	7	8	9	10	11	12	Up-hole end (1)
Thickness measured (in.)	0.121"	0.111	0.107	0.101	0.083	0.068	0.056	0.056	0.082	0.087	0.105	0.120	0.120	0.133

(1) Measured at approximately 12" from the central portion on each side

Cleanout – 1-3/4" – CT90

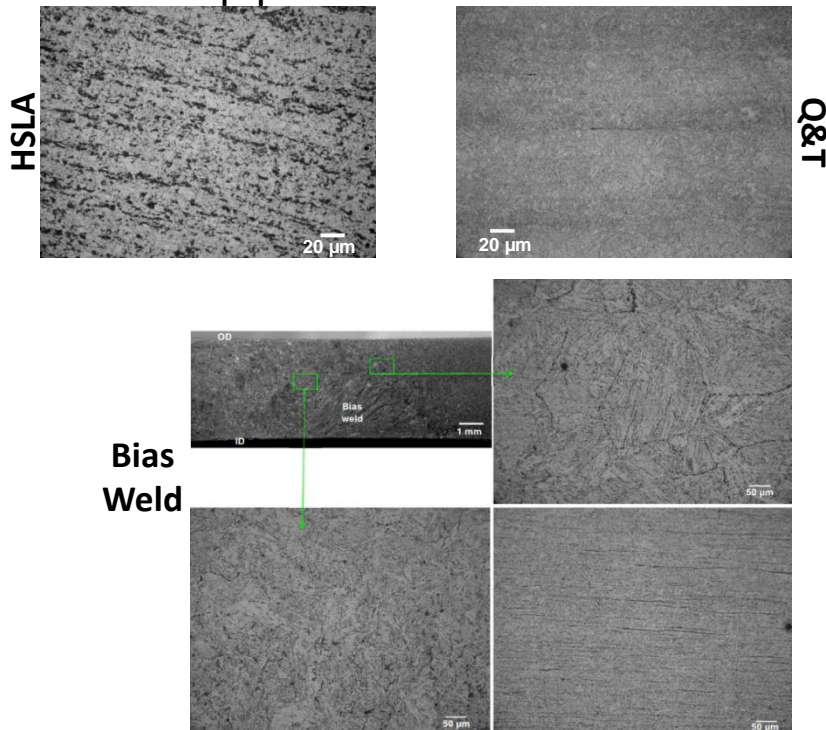
Acid job – 1-1/2" – CT80

CT string failure analysis process – Metallographic analysis

- With the information gathered from the previous stages normally there is a good idea of what caused the failure.

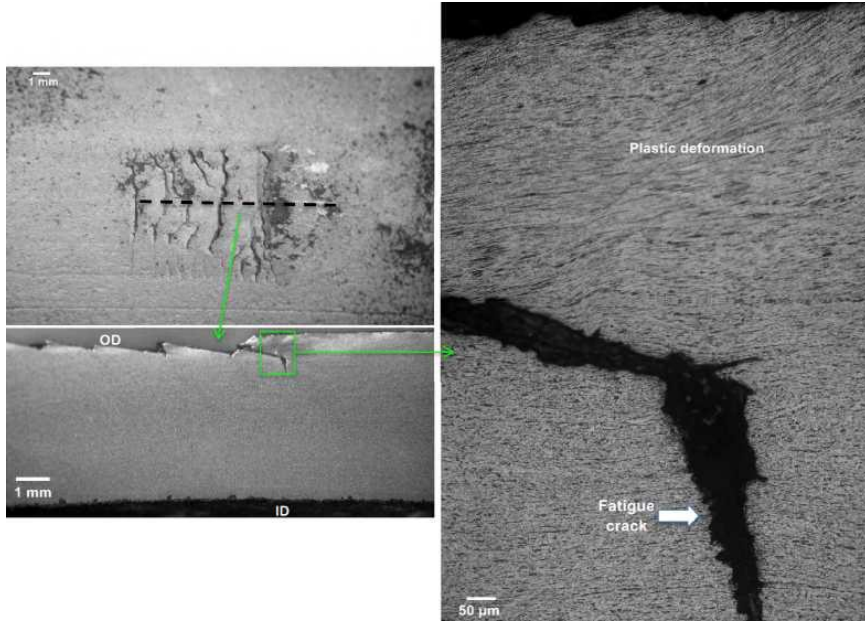


- Check pipe microstructure is OK:

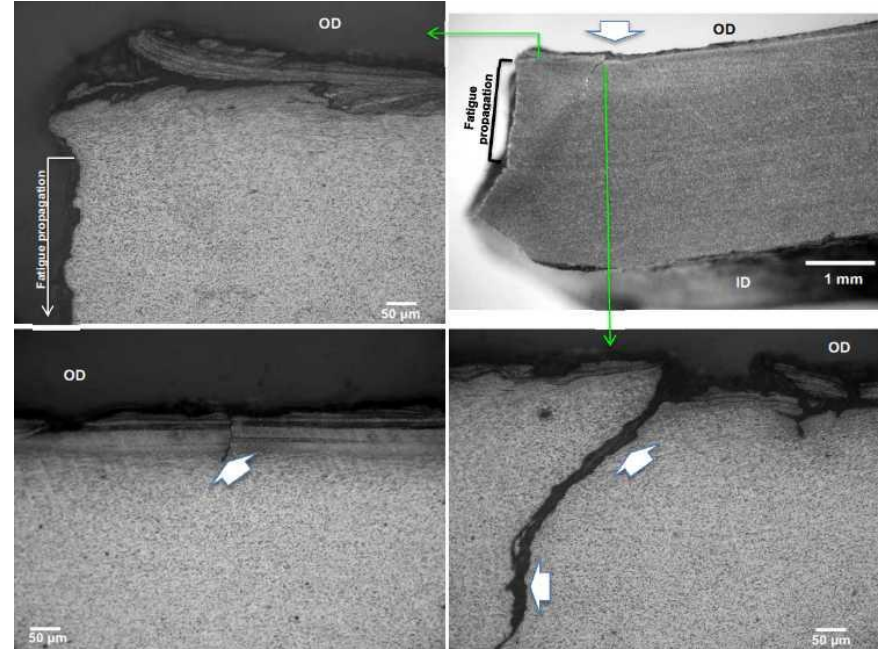


CT string failure analysis process – Metallographic analysis

- Mechanical damage: confirm plastic deformation at damage:



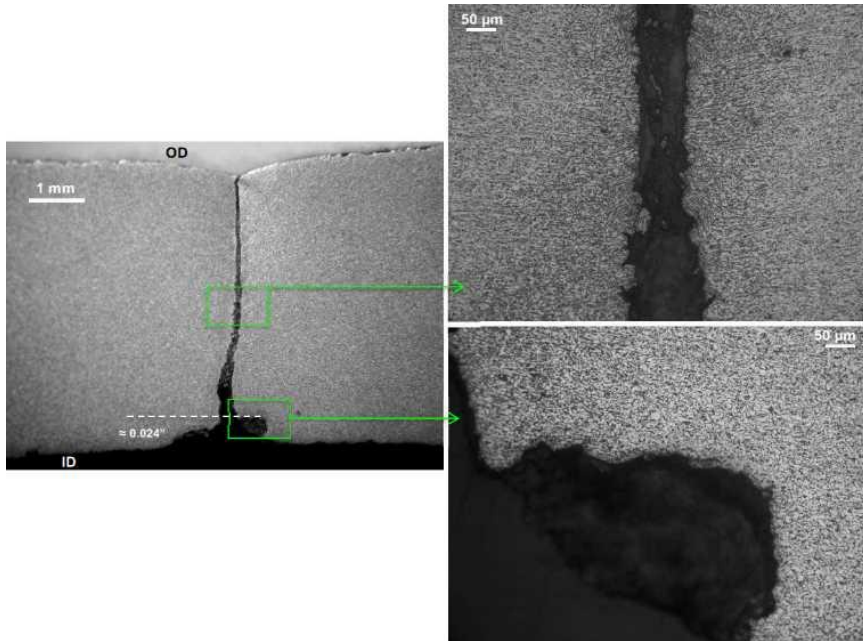
Longitudinal plow mark



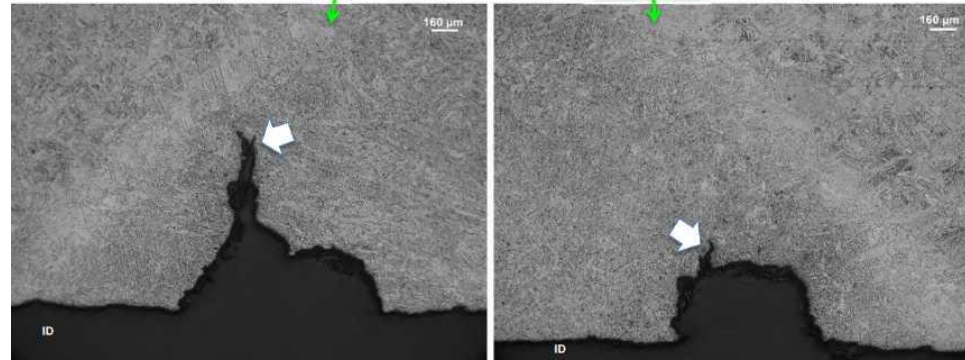
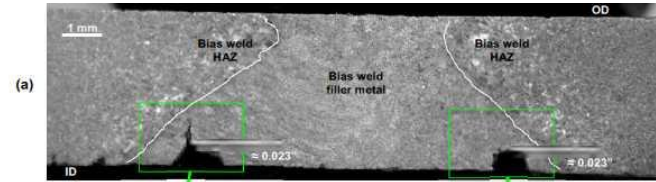
Pipe crushing

CT string failure analysis process – Metallographic analysis

- Corrosion: corrosion depth / metallurgy at corrosion:



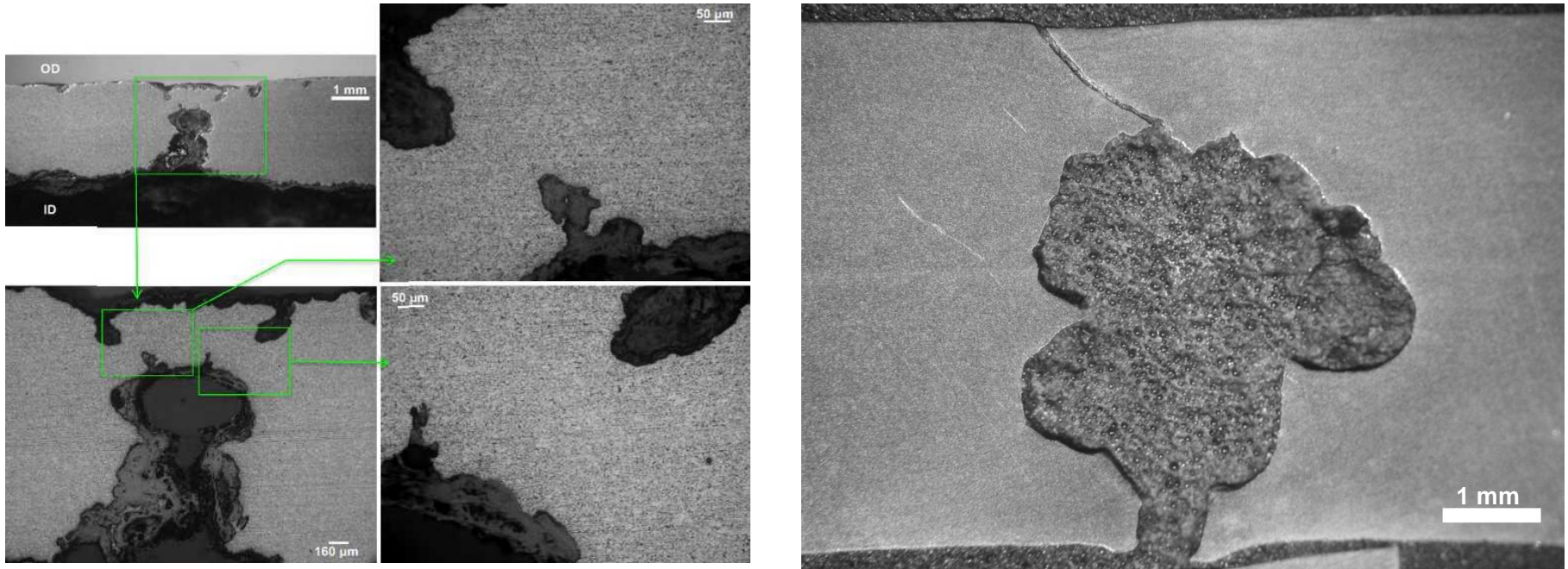
Internal pit



Internal pitting at bias weld

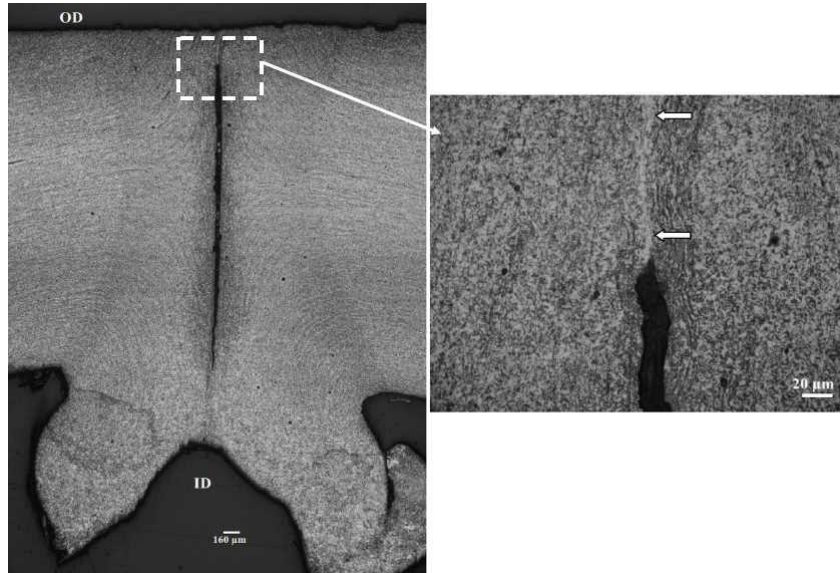
CT string failure analysis process – Metallographic analysis

- MIC: pitting shape: normally “cavernous”, deep, and very aggressive:



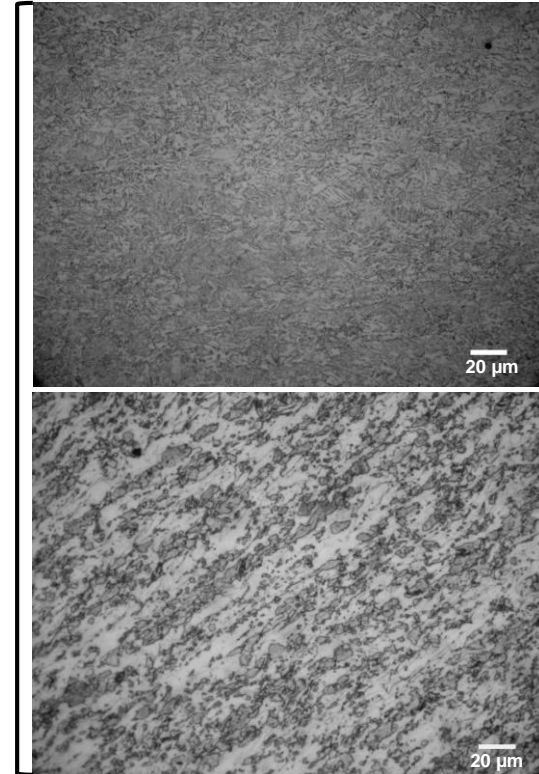
CT string failure analysis process – Metallographic analysis

- Manufacturing flaw:



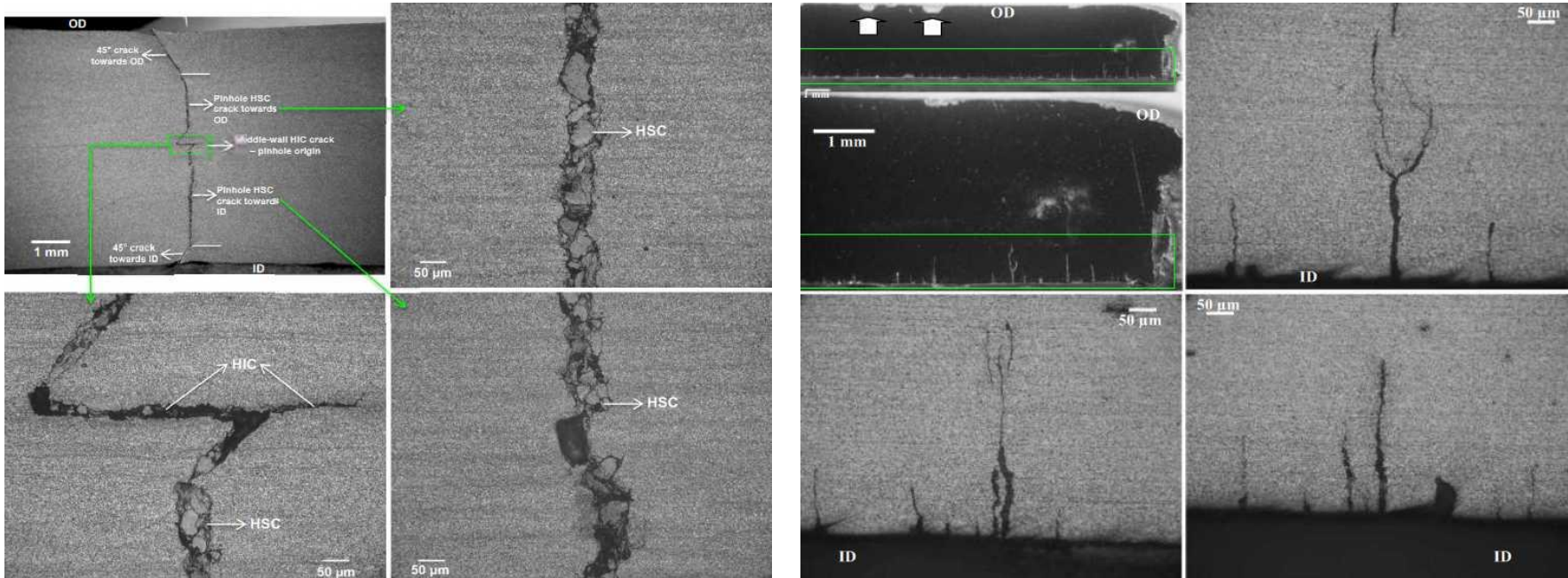
“Cold weld”

Abnormal microstructures



CT string failure analysis process – Metallographic analysis

- Environmental cracking:



H2S cracking

Caustic cracking

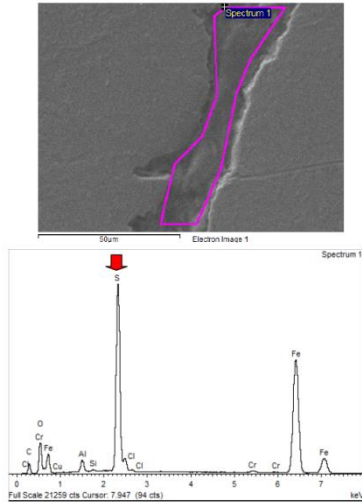
CT string failure analysis process – EDS

- EDS: corrosion products / foreign particles

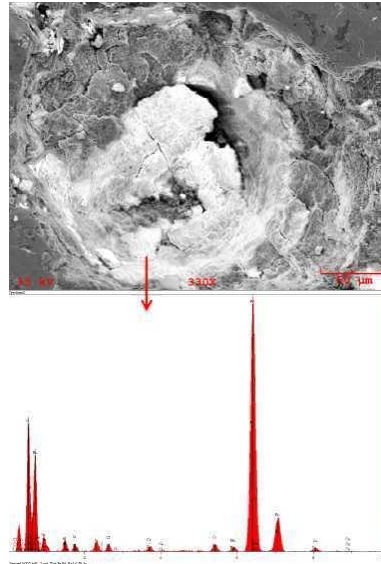
Spectrum processing:
Peak possibly omitted: 7.456 keV
Processing option: All elements analyzed (Normalised)
Number of iterations = 4

Standard:
C CaCO₃ 1-Jun-1999 12:00 AM
O SiO₂ Pella 9-Mar-2017 11:49 AM
Al Al Pella 9-Mar-2017 12:05 PM
Si SiO₂ Pella 9-Mar-2017 11:49 AM
S FeS₂ 1-Jun-1999 12:00 AM
Cl KCl 1-Jun-1999 12:00 AM
Cr Cr 1-Jun-1999 12:00 AM
Fe Fe 1-Jun-1999 12:00 AM
Cu Cu 1-Jun-1999 12:00 AM

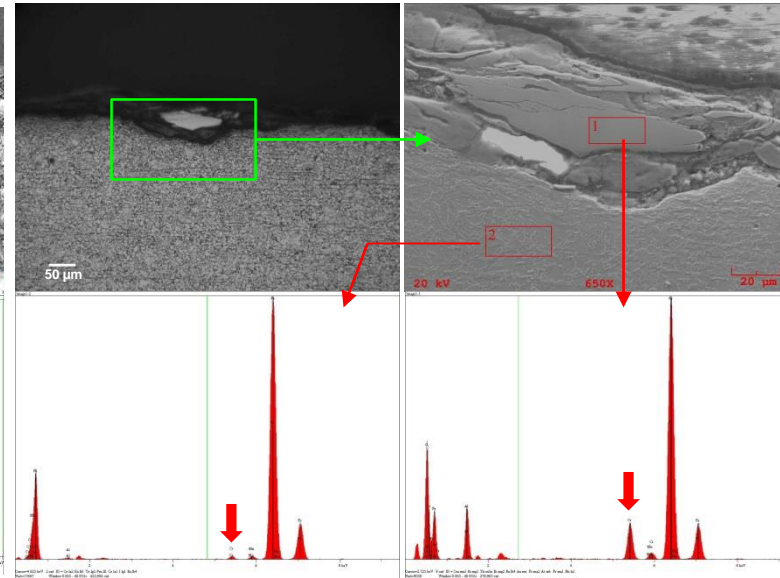
Element	App. Conc.	Intensity Corr.	Weights	Weights Sigma	Atomics
C	3.91	0.2217	24.62	0.49	48.35
O	5.43	0.6534	11.60	0.17	17.11
Al	0.46	0.6367	1.01	0.03	0.88
Si	0.06	0.7480	0.11	0.02	0.09
S	13.99	0.8712	29.39	0.17	16.48
Cl	0.13	0.6274	0.29	0.03	0.19
Cr	0.27	0.9672	0.39	0.03	0.18
Fe	24.82	0.8782	39.43	0.28	16.66
Cu	0.09	0.7967	0.16	0.05	0.06
Totals			100.00		



EDS within a crack – (S)



EDS within external pit – (Fe, O)

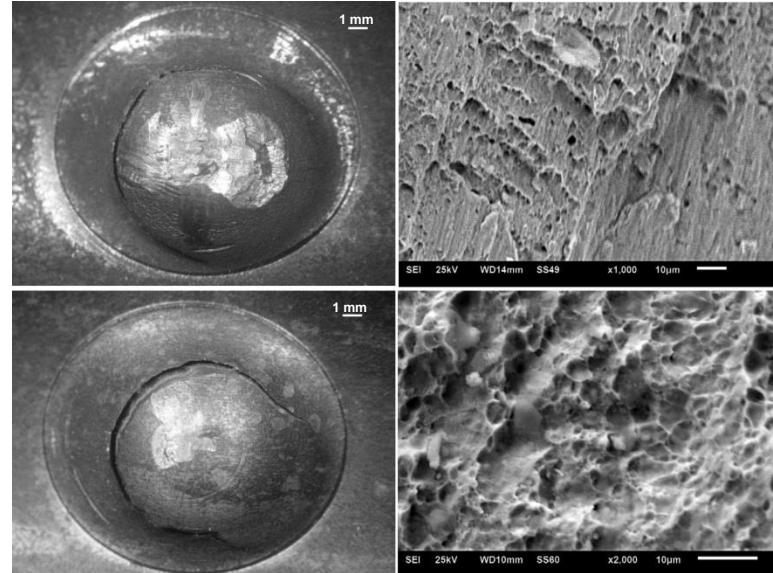
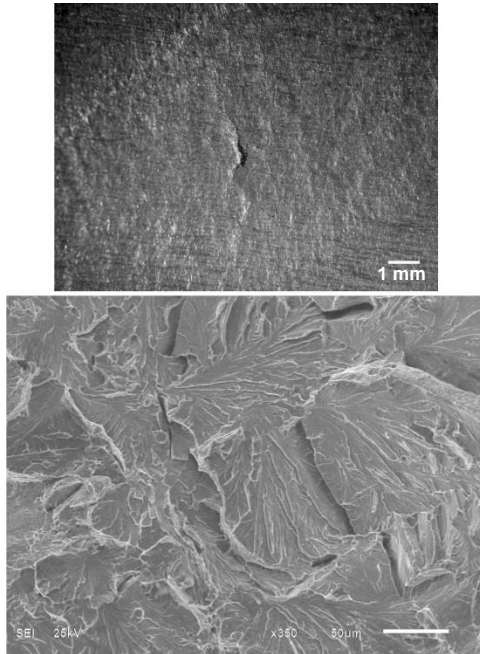


EDS on particle – Higher Cr than base metal

CT string failure analysis process – SEM Fractography

- SEM fractography: confirming fracture propagation mode: brittle (cleavage/intergranular) or ductile (dimples).

Cleavage on secondary crack (after opening) – MIC failure



Cracks on dimple on connection –
Elongated dimples (shear) on cracks

CT string failure analysis process – Tension test

SPE 38412

Determining the
A. Crabtree, SPE, BJ Se

SPE 38412

- 3.d. Conduct one unloading and reloading cycle at approximately 0.8% of strain to obtain the elasticity modulus as schematically shown in Figure 11.
- 4.b. Determine the Yield Strength by intercept of the tensile curve with the 1% offset line drawn at the angle of the elastic reloading line obtained in step 3d.

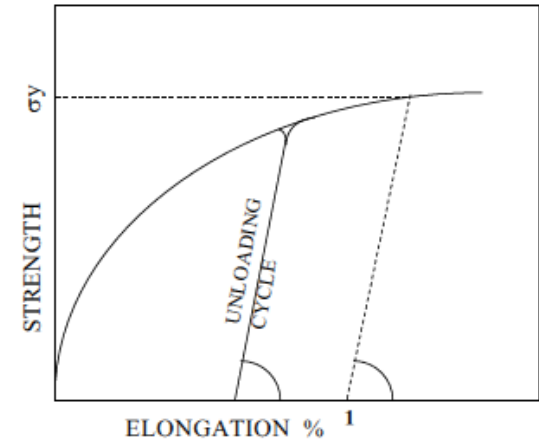
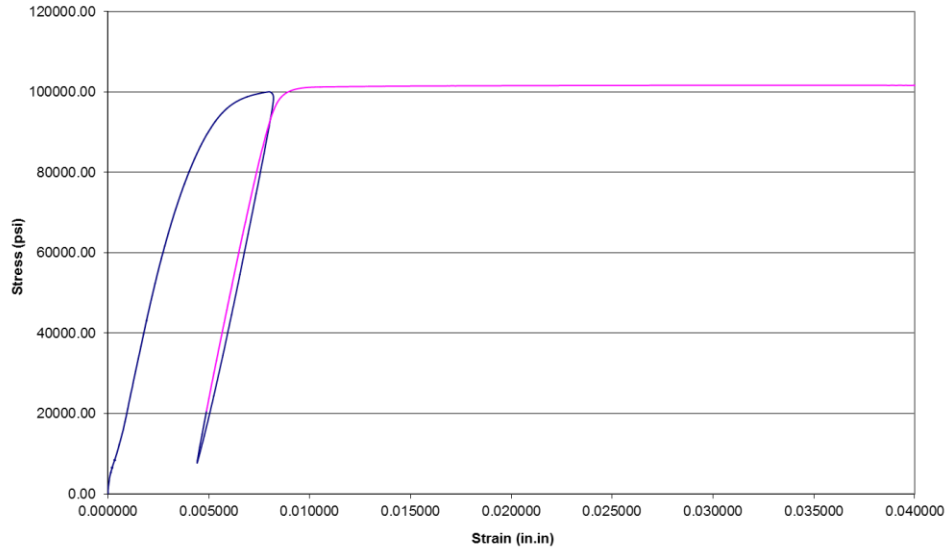


Figure 11. Schematic showing a full body tensile test procedure for determining Yield Strength and modulus of elasticity of bent pipe.

... length.

CT string failure analysis process – Tension test

207-0087786 Baker Hughes
Sample 1



TENSILE TEST

Client: Baker Hughes Canada Company
Address: 6620-36 St. SE
Calgary, AB
T2C 2G4

Attention: Tomas Padron

Sample Description: 1-3/4 in. OD ± 0.125 in. WT Nominal Coiled Tubing

Specimen Type & Preparation: As received tube
Test Procedure: ASTM A370 / SPE 38412 Appendix III
Governing Specification: No governing specification stipulated

Test Result: As reported below

Acme Specimen ID :	Test Results		Gov. Spec. Requirements	
	Imperial (ksi)	Metric (MPa)	Imperial (ksi)	Metric (MPa)
Yield Strength (1% Offset Method) *	102	700	N/S	N/S
Ultimate Tensile Strength *	102	700	N/S	N/S
Elongation (%)	20		N/S	

Acme Specimen ID :	Test Results		Gov. Spec. Requirements	
	Imperial (ksi)	Metric (MPa)	Imperial (ksi)	Metric (MPa)
Yield Strength (1% Offset Method) *	101	700	N/S	N/S
Ultimate Tensile Strength *	102	705	N/S	N/S
Elongation (%)	24		N/S	

N/S = Not Specified
* Calculated values are based on nominal tubing dimensions.

Reviewed By:

Tested By:

Specimens will be
disposed of 60 days
after test date.



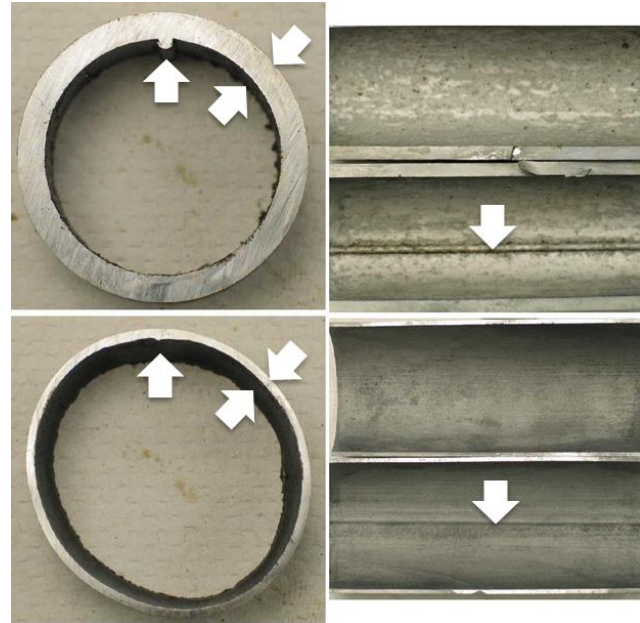
CT Failures Statistics – Terminology

Storage-corrosion: corrosion damage caused by the accumulation of corrosive fluids (within or outside the string) while it remains in storage for long periods.



Internal storage-corrosion example

Acid internal-corrosion example



Corrosion-operations: corrosion damage caused by the action of fluids pumped or the well environment during operations

CT Failures Statistics – Terminology

Manufacturing flaw: premature failure associated with issues originated during the manufacturing process

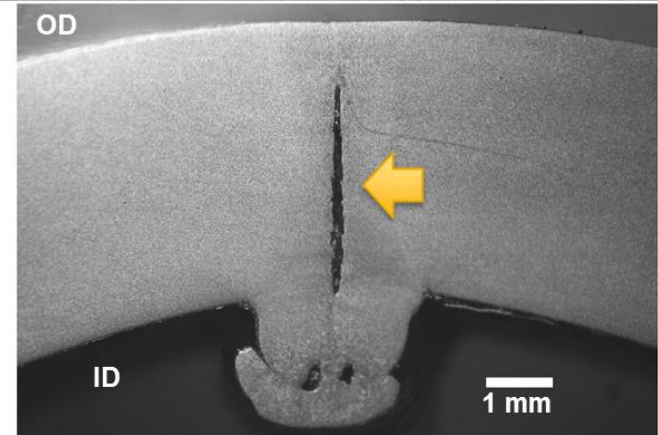
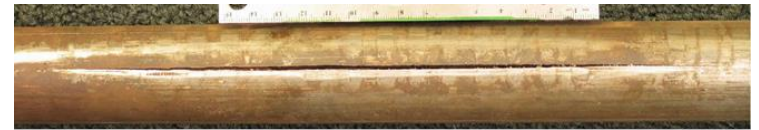
Longitudinal plow mark



External dent



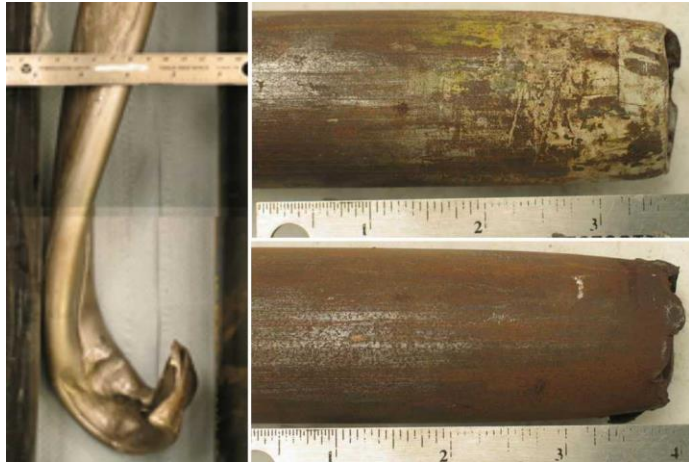
Mechanical damage: premature fatigue failure that starts at external damage caused by mechanical means.



“Cold weld” example

CT Failures Statistics – Terminology

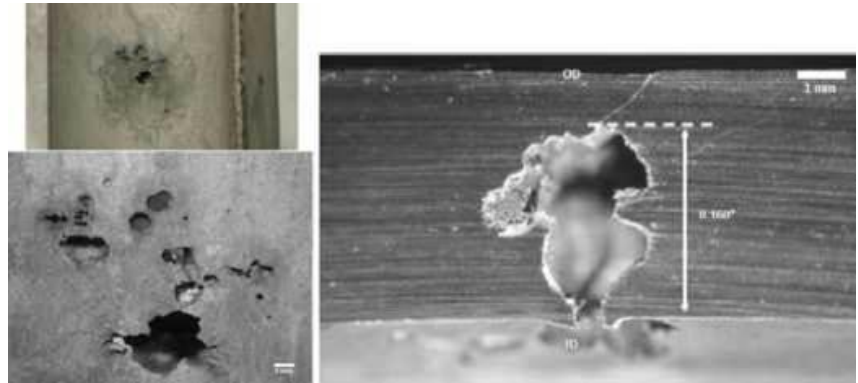
Human error: failure associated with errors during the string operation.



Buckling

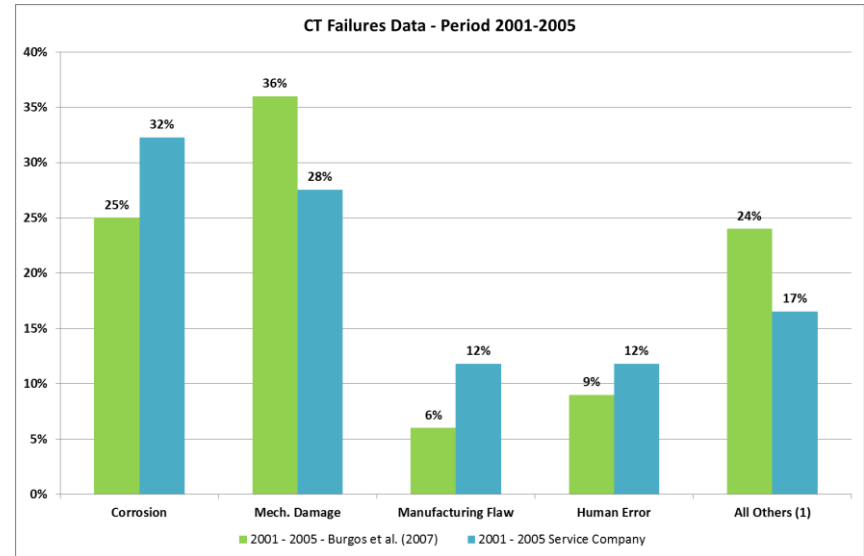
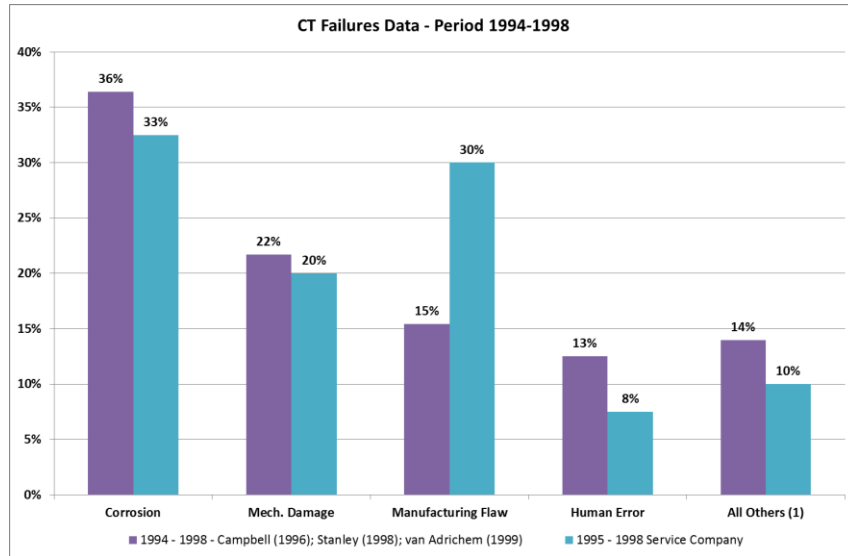
Overload

Internal MIC



MIC (Microbiological influenced corrosion): corrosion failure due to the presence of certain specific type of bacteria within the fluid in contact with the pipe.

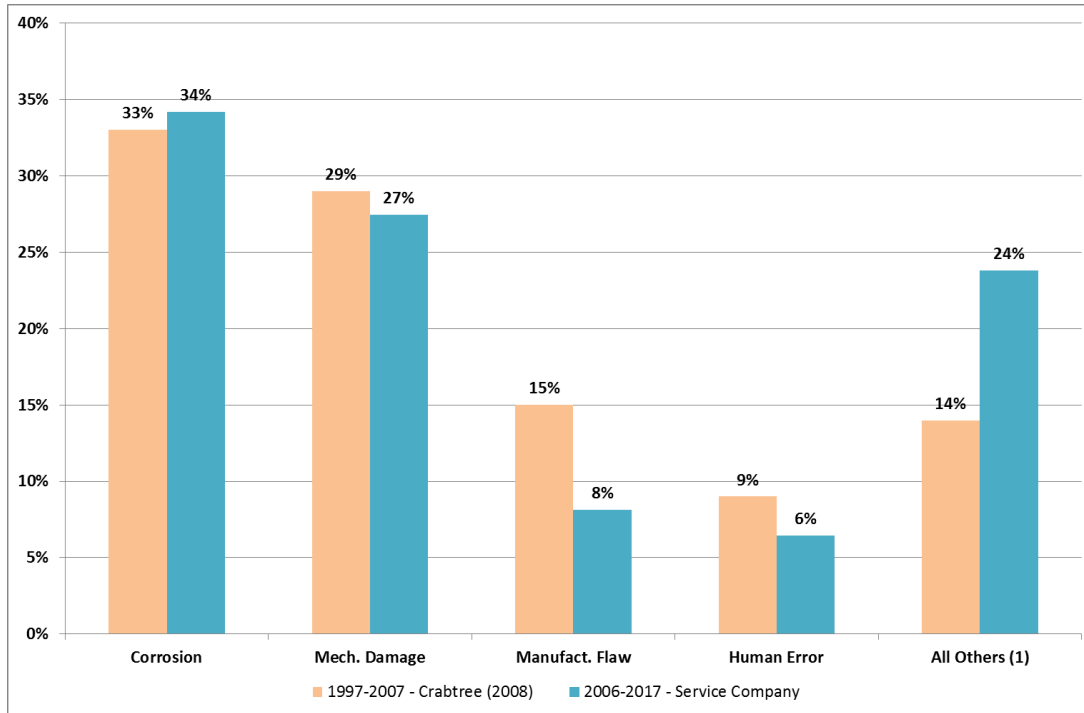
CT Failures Statistics – Period 1994-2005



(1) All Others includes: fatigue, erosion, H2S failure, field welding, ext. abrasion, unknown

- CT Failures trend is similar for the CT industry
- Main causes: Corrosion / Mechanical damage / Manufacturing flaw / Human error
- These causes represent around 80% to 90% of CT failures

CT Failures Statistics – Period 2006-2017 vs. Previous Periods

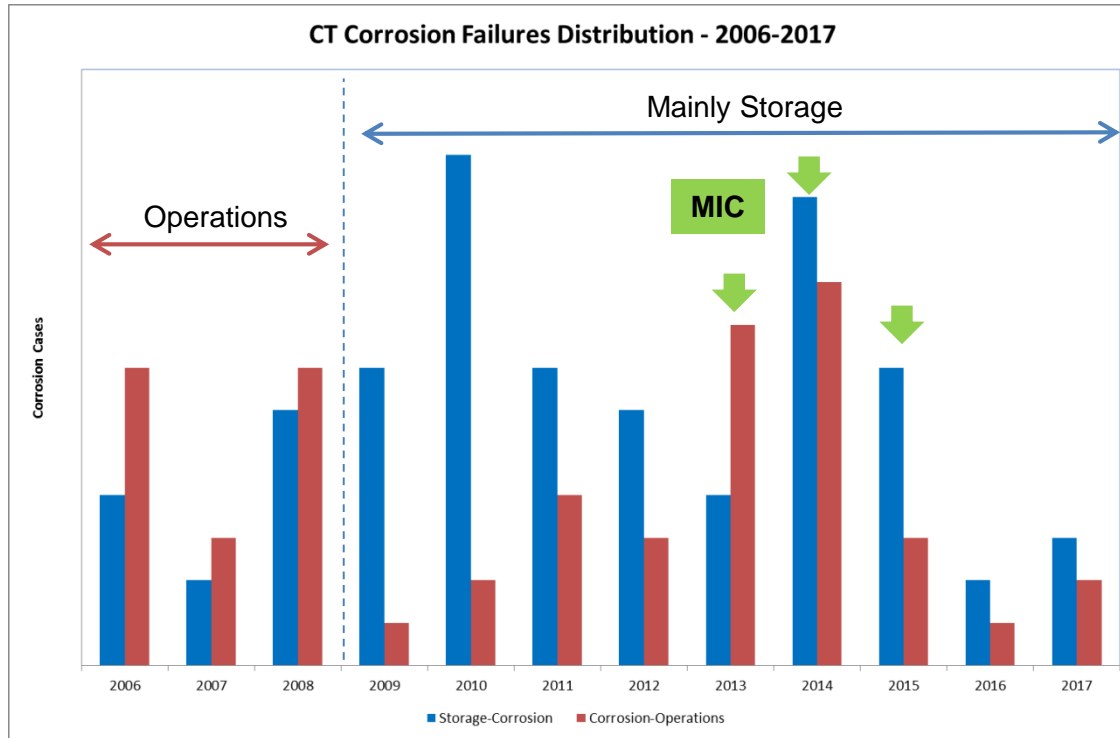


(1) All Others includes: fatigue, erosion, H2S failure, field welding, ext. abrasion, unknown

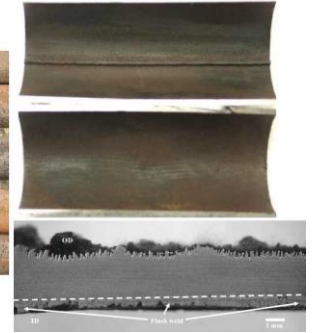
4 main CT failures causes have remained the same:

- Corrosion ($\approx 30\%$)
- Mechanical damage ($\approx 30\%$)
- Manufacturing flaw
- Human error

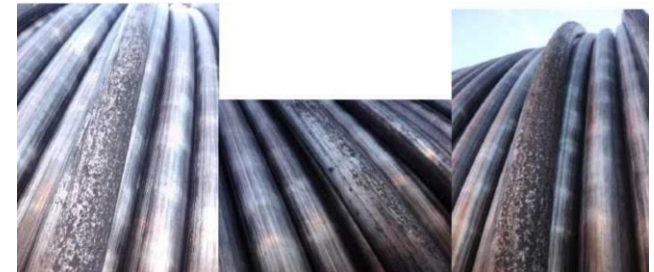
Main Failures Causes Review: Corrosion ($\approx 30\%$)



Corrosion-Operations

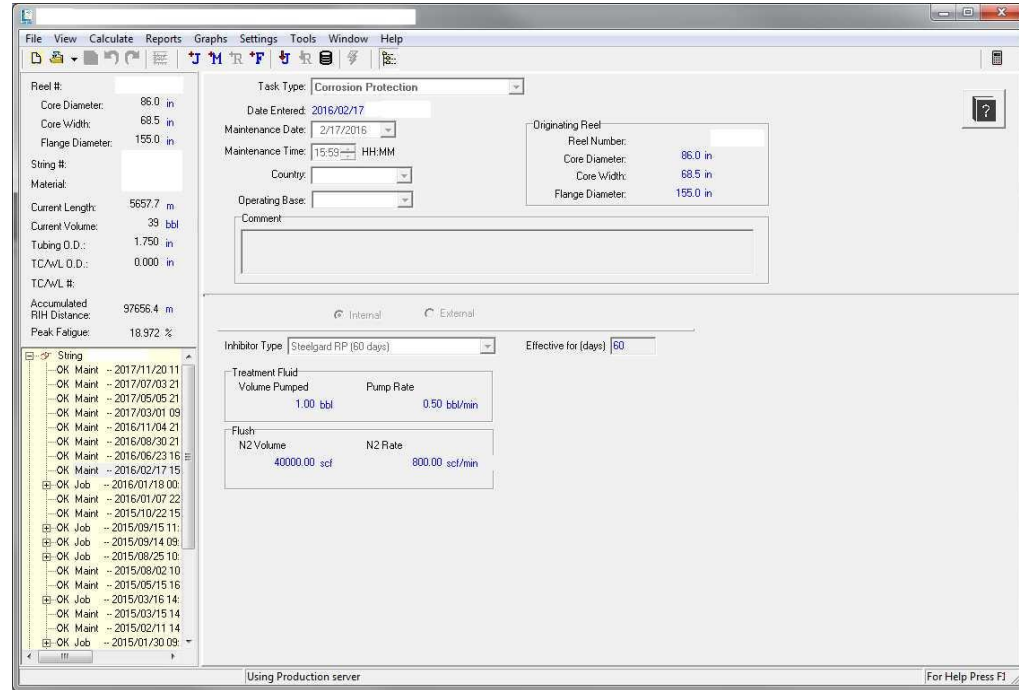


Storage-Corrosion



Main Failures Causes Review: Corrosion (≈30%)

- Mitigation measures - Storage-corrosion:
 - Eliminating residual fluids
 - Application of corrosion inhibitors (internally/externally)
 - Records kept within the string management system



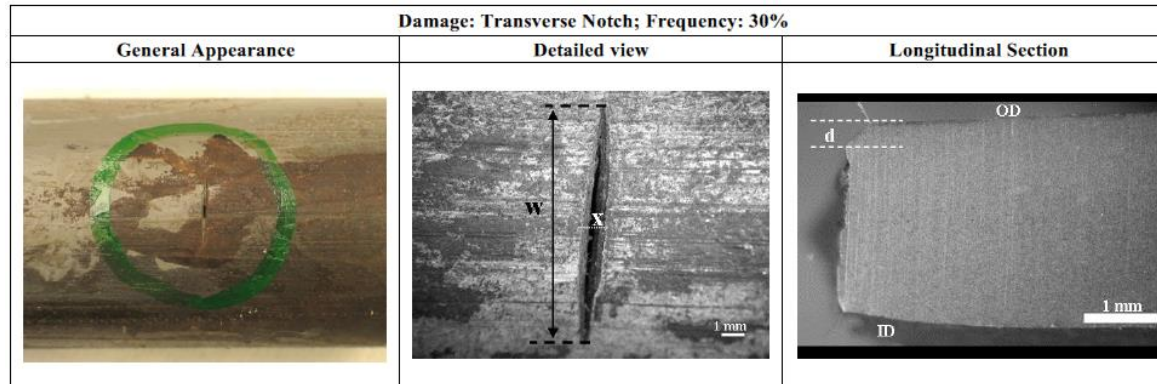
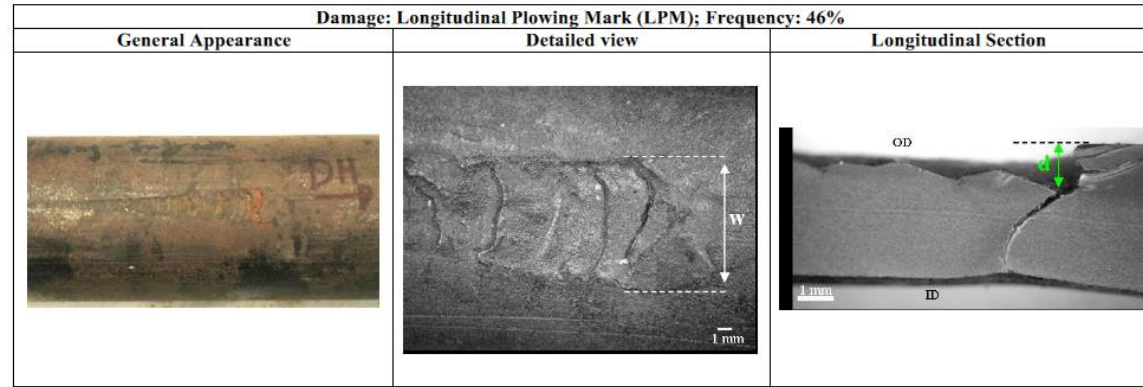
Main Failures Causes Review: Mechanical Damage ($\approx 30\%$)



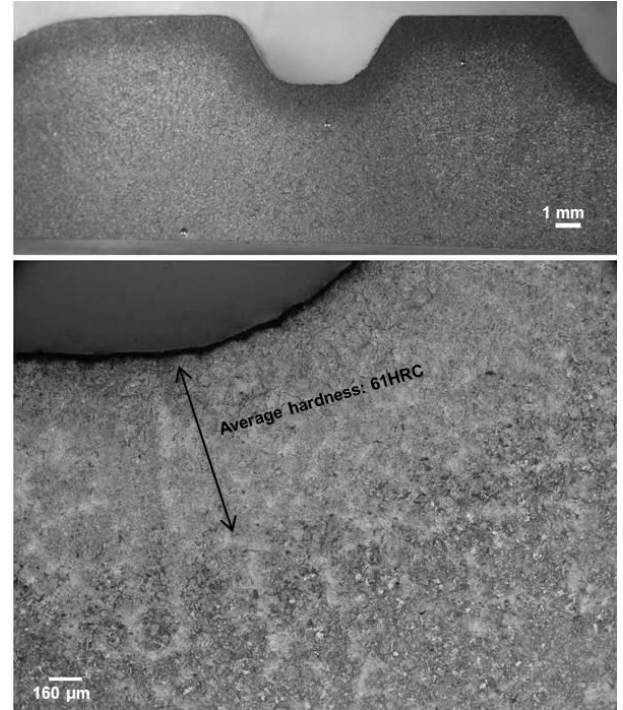
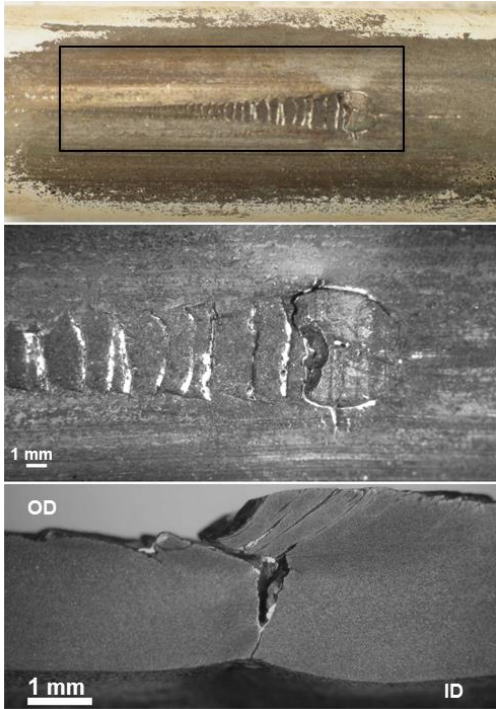
- Normally caused by the action of the surface equipment.
- Can be very diverse.
- Stress/strain concentration point

Main Failures Causes Review: Mechanical Damage ($\approx 30\%$)

Most frequent types of mechanical damage (2006-2017):

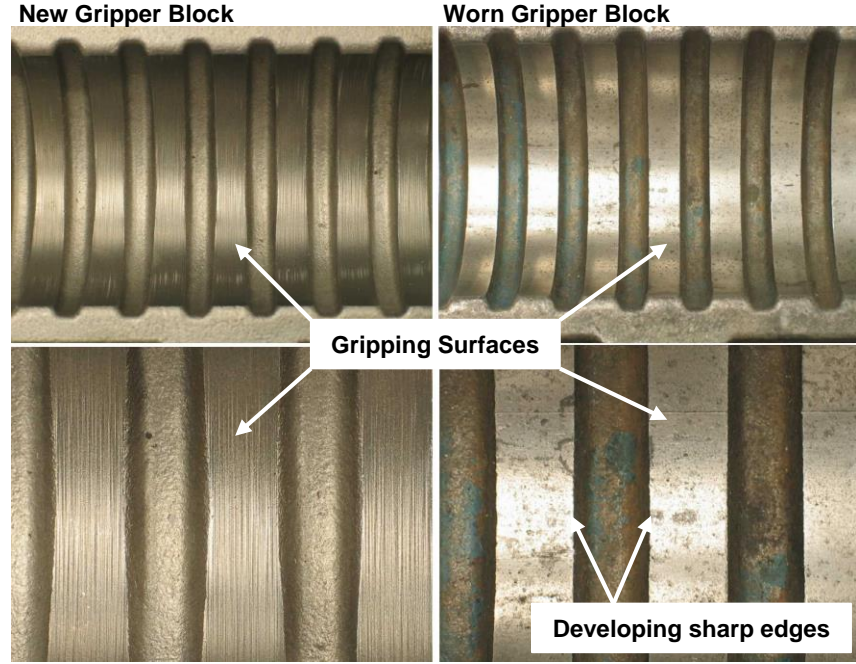


Main Failures Causes Review: Longitudinal Plowing Marks (LPM)

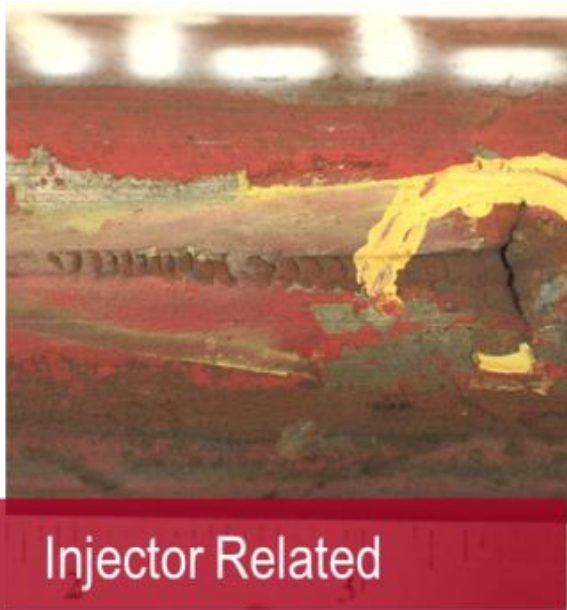


Main Failures Causes Review: Longitudinal Plowing Marks (LPM)

Frequently associated with worn gripper blocks



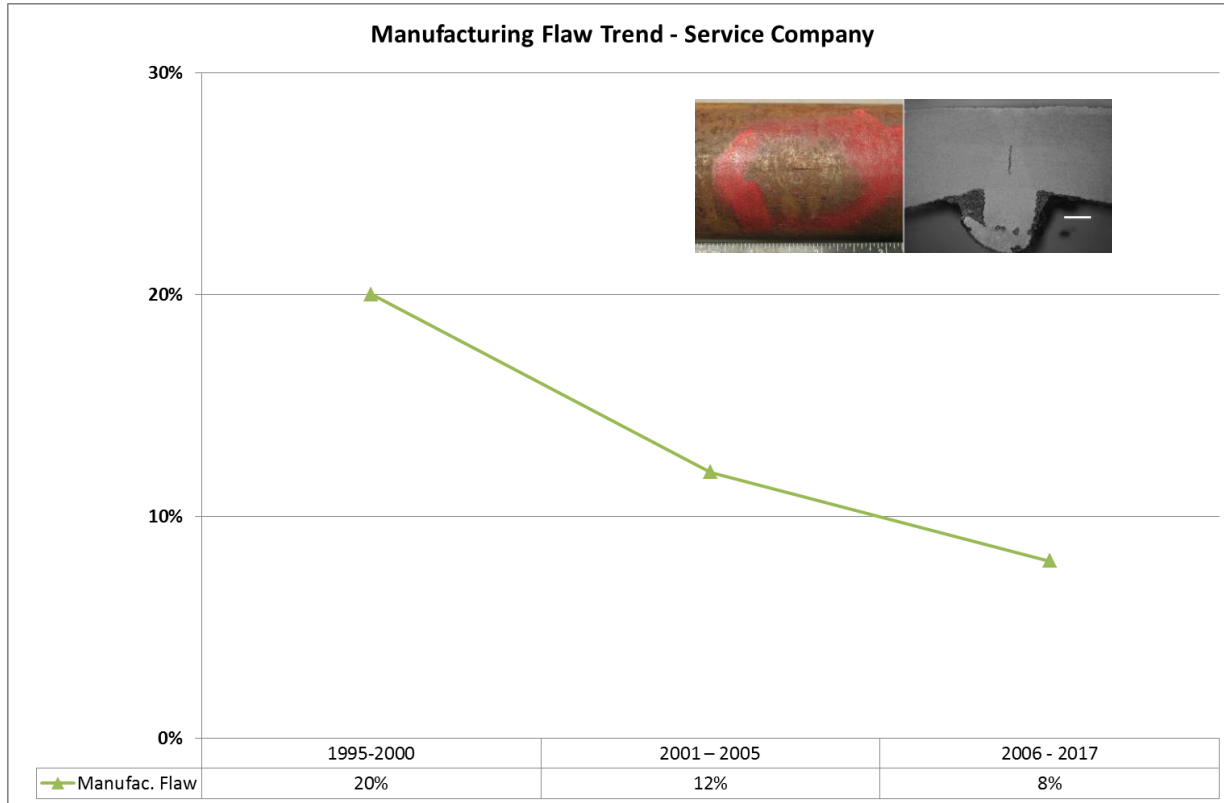
Main Failures Causes Review: Longitudinal Plowing Marks (LPM)



Some mitigation actions for LPM:

- Replacing “smooth” gripper blocks based on OEM recommendations
- Coating gripper blocks with tungsten carbide
- Inspect gripper blocks prior mobilization for the presence of debris in the grooved gripper blocks

Main Failures Causes Review: **Manufacturing Flaw**



Main Ideas

- CT Failures occur and in many cases it is worthy to perform failure analyses to establish the cause(s) based on data/evidence








Main Ideas

CT failure analysis:

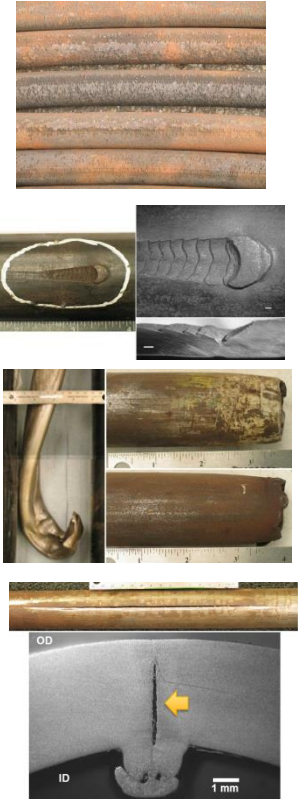
Logical process of examination to establish the failure cause(s) based on evidence collected and the use of engineering principles.



- Most common CT failure analyses include the following stages:
 - Sample(s) collection/preservation
 - Collection of data regarding failure/CT string 
 - Visual/stereoscopic examination 
 - Dimensional inspection 
 - Metallographic analysis 
 - Results analysis and report preparation 

Main Ideas

- Data allow inferring that the main CT Failures causes are similar for the CT industry.
- No significant change was observed on the CT failures causes for the periods 1994-2005 and 2006-2017:
 - Corrosion
 - Mechanical damage
 - Manufacturing flaw
 - Human error
- These causes represented around 80% - 90% of the CT failures



Acknowledgements

ICoTA Canada
Baker Hughes a GE Company
Steven Craig

Thank you

Questions?

